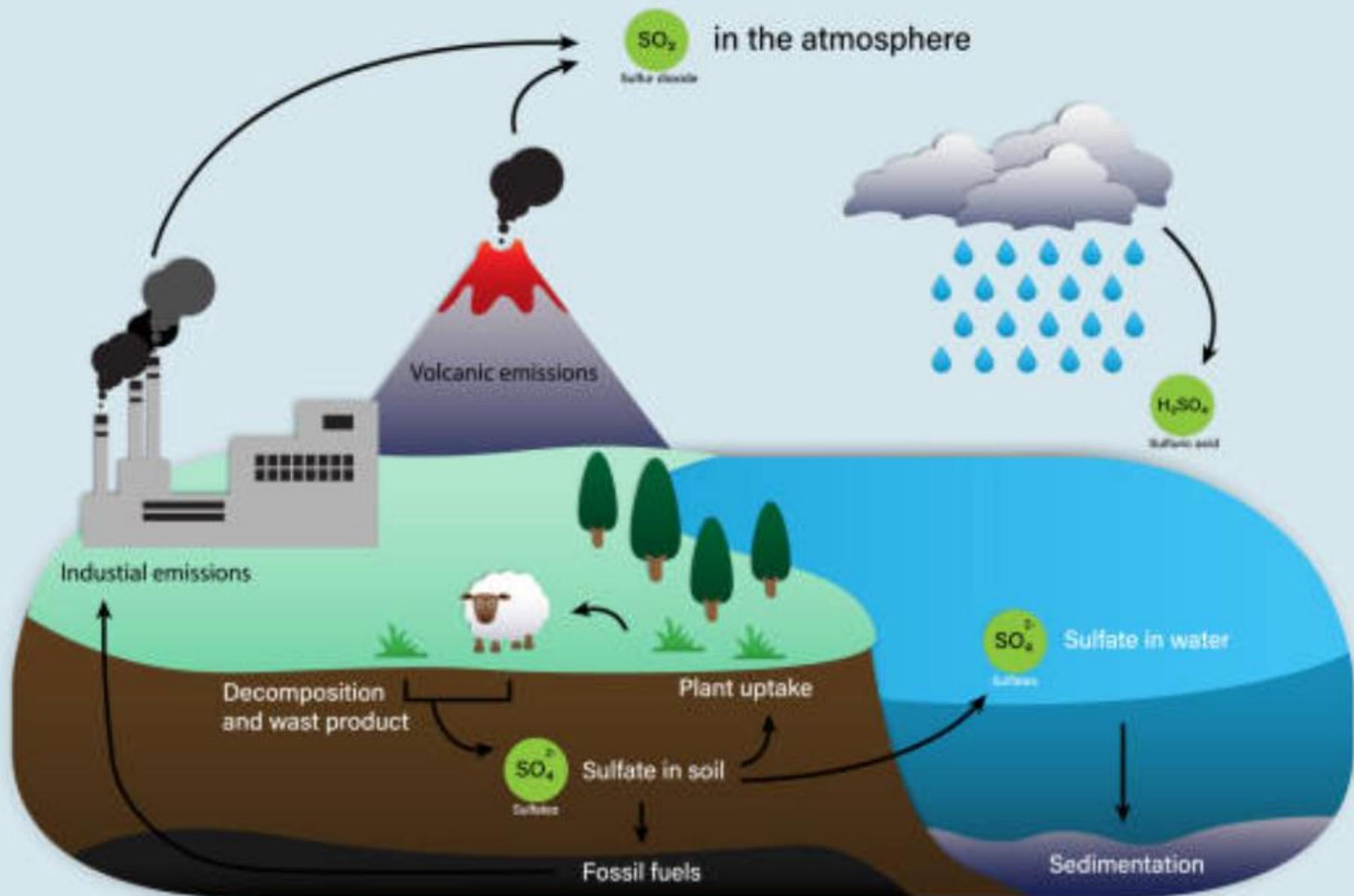


# Hydrocarbon Processing

- Desuphurisation
- Diesel quality improvement



# Sulfur Cycle



# Composition: types of **impurities**

- **Heteroatom** components

- **Sulphur compounds**

- Elemental sulphur
- Hydrogen sulphide
- Mercaptanes
- Sulphides-disulphides
- Thiophen and derivatives

- **Nitrogen compounds**

- Amines
- Nitriles
- Pirrols

- **Oxygen compounds**

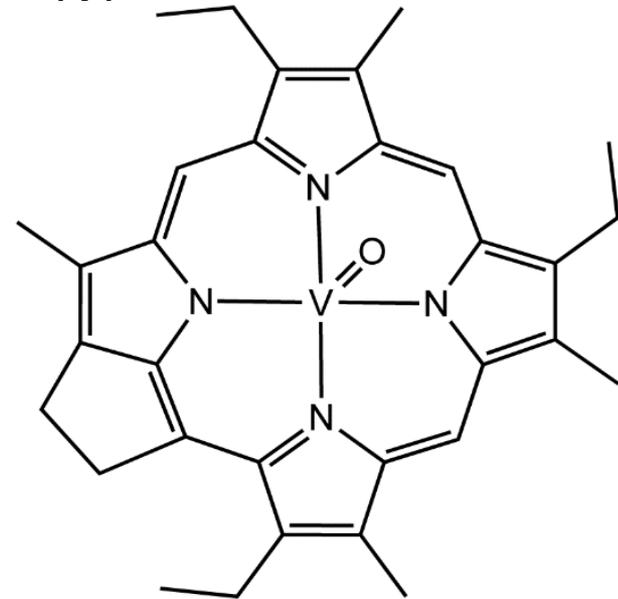
- Organic acids
- Phenols

- **Inorganic ions**

- Solved in the dissolved water
- $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{HCO}_3^-$ , etc.

- **Organic metal complexes**

- Mainly nickel (Ni) and vanadium (V)

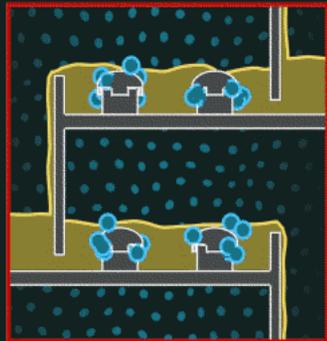


# DISTILLATION

Crude oil contains a variety of **hydrocarbons** that have different boiling points. To separate these compounds, the oil is first sent to a boiler where it is heated into a super-hot mixture of liquid and vapour called the feed.

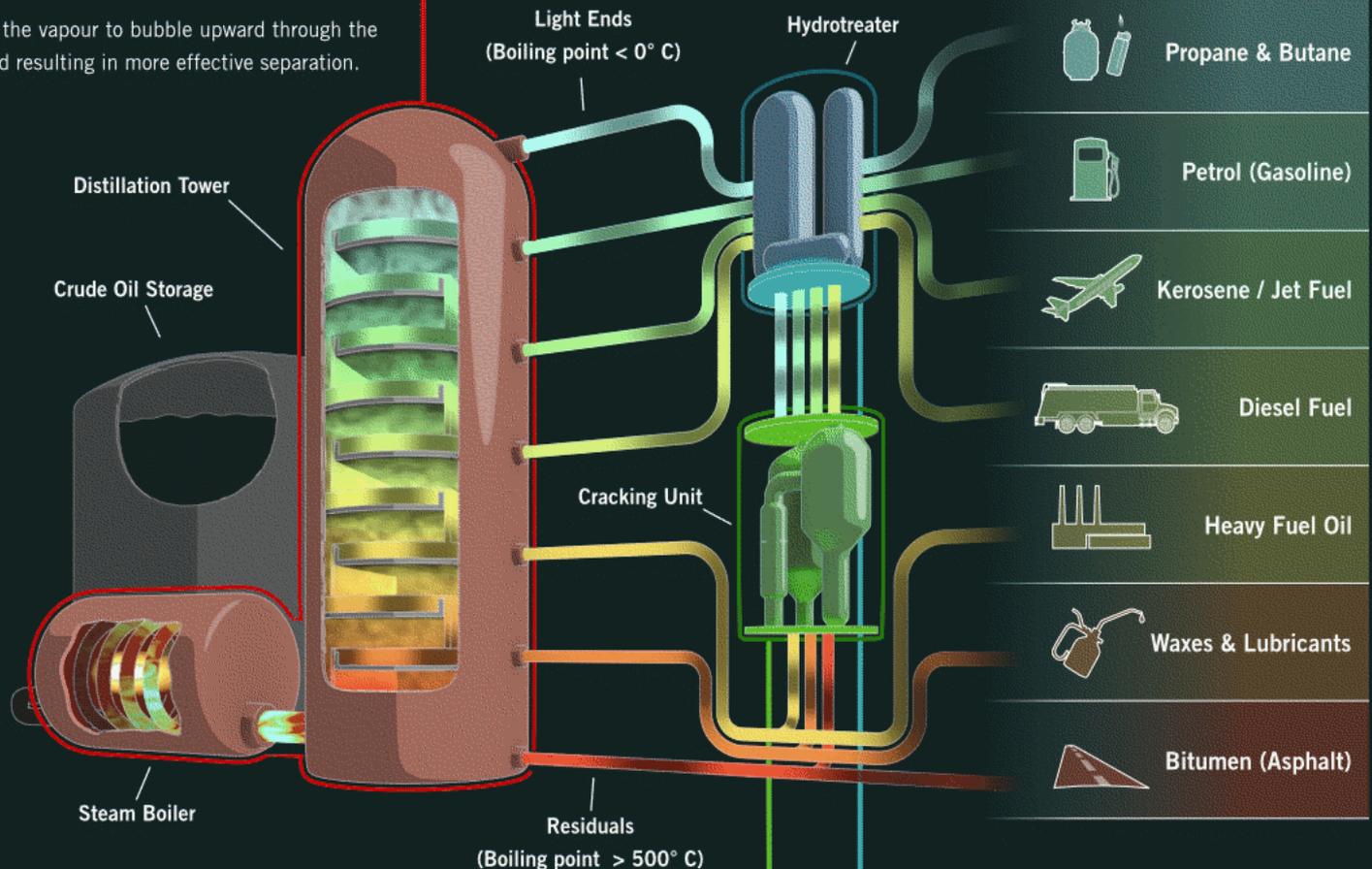
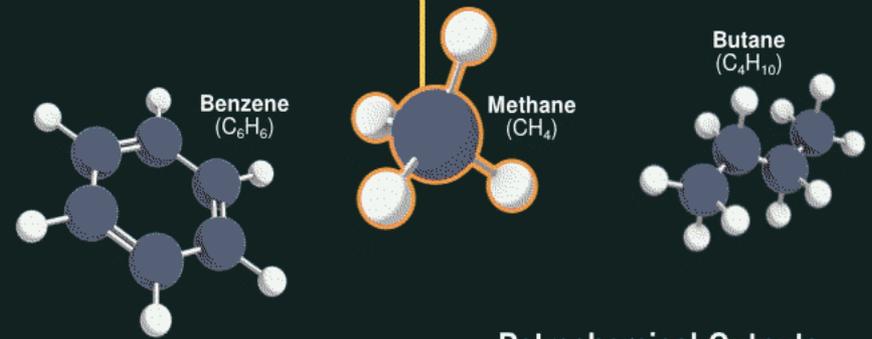
The mixture is then fed into a **distillation tower**. In here, the compounds with a lower boiling point rise up as vapours, while the compounds with a higher boiling point fall downwards as liquids.

The tower contains trays that allow the vapour to bubble upward through the liquid, helping to exchange heat and resulting in more effective separation.

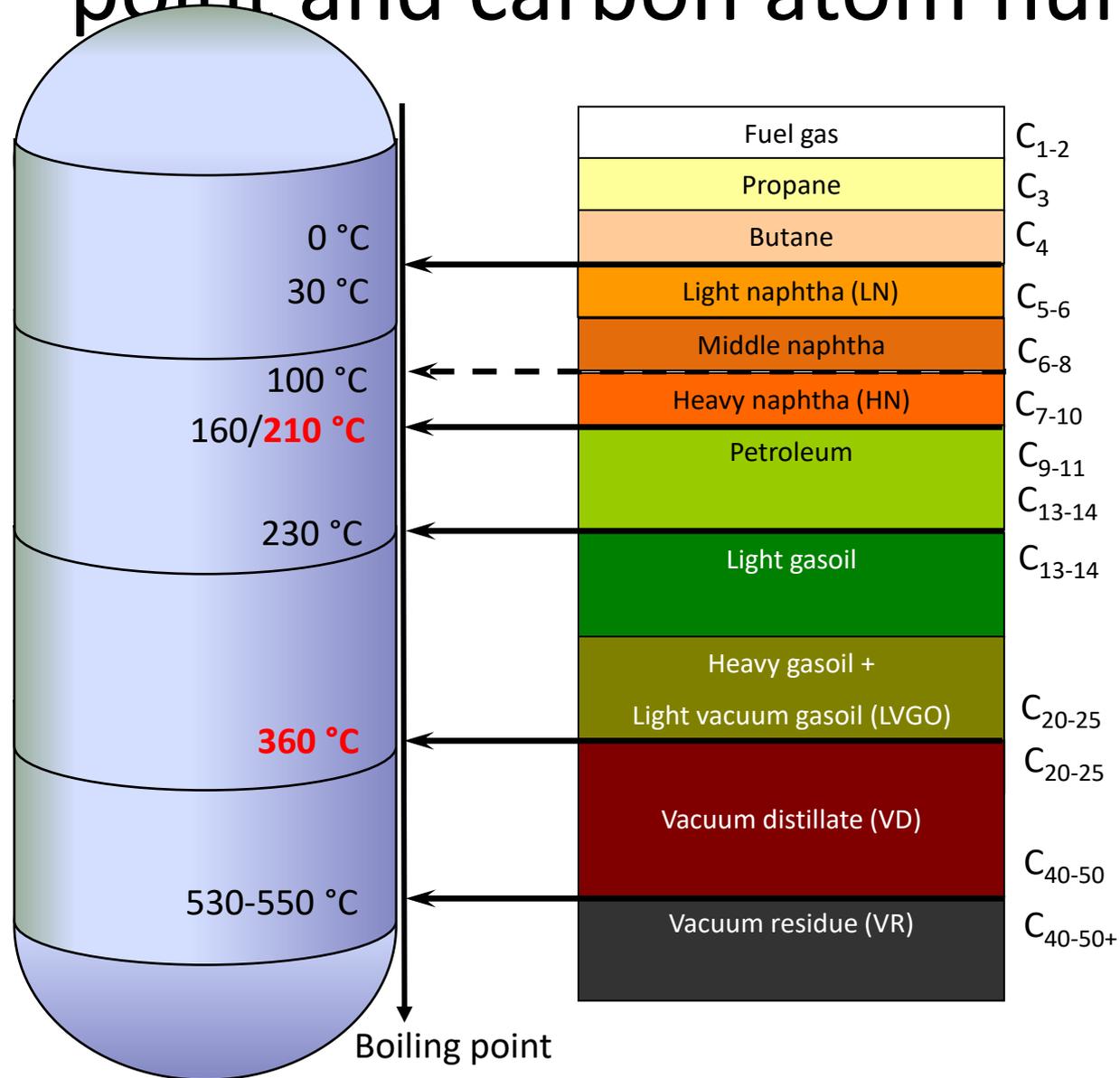


The distilled products are then piped off from the different levels of the tower. These separated products are called **fractions** or **distillates**.

This process may take place along multiple distillation towers.



# Crude oil fractions according to boiling point and carbon atom number



# 1. Desulphurization



# Importance of desulphurisation

- To meet **product quality specification**
  - Gasoline, diesel: 10 ppm S content
- To prevent **catalyst poisoning** during downstream processing
  - pl. catalytic reforming (CCR): platinum catalyst
- To prevent **corrosion**
  - Carbon steel equipment, heat exchanger protection
- To protect **exhaust gas catalyst** in cars
  - Platinum catalyst as well as CCR
- General **environment, health protection**
  - Acidic rain, etc.

# Desulphurisation of **fuel gas**

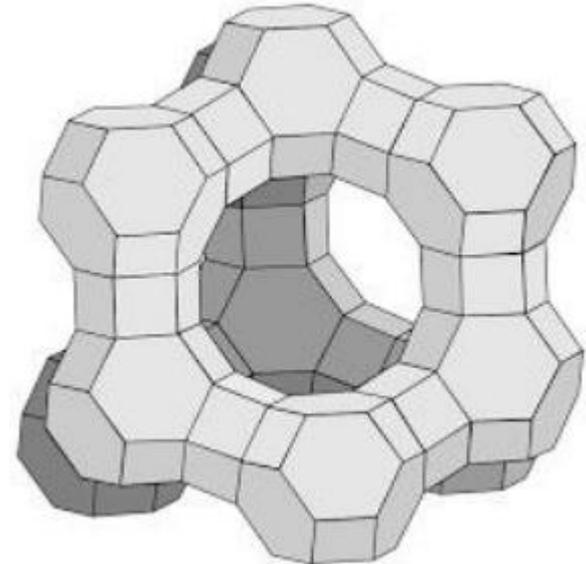
- **Definition:** fuel gases are the gaseous intermediate streams produced during crude oil processing, which consists basically only methane and ethane components
- Their **marketisation is not economic** (low amount, expensive to separate), therefore they are used internally in furnaces (burning)
- **Principle** of desulphurisation: gas/liquid extraction (amine washing)
  - Absorption – desorption
  - **Absorbents:** ethanol-amines
  - Details later under the title „sulphur recovery”

# LPG desulphurisation

- **LPG:** Liquefied Petroleum Gases
- Examples of **sulphur species** in LPG
  - Carbonil-suphide (COS; bp.: -50°C)
  - Methyl-mercapthan (CH<sub>3</sub>SH; bp.: +6°C)
- **Technologies**
  - Removal with molecular sieves
    - **straight-run LPG** (straight-run: stream from the primary distillation)
  - Removal with caustic
    - Cracked, **olefinic LPG**

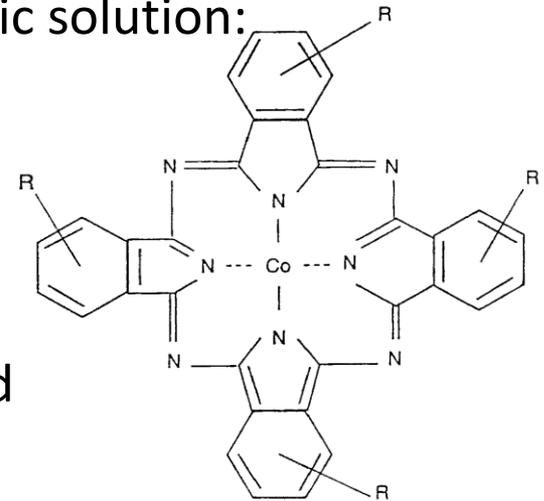
# LPG desulphurisation with **molecular sieves**

- **Theory** of desulphurisation: adsorption (liquid/solid extraction)
- **Advantage:** simple operation, cheap adsorbent
- **Disadvantage:** not good for olefinic fractions
- Molecular sieves used as adsorbent
  - eg. **13X**, 5A zeolites
  - Molecular sieves: strictly regular pore size mineral

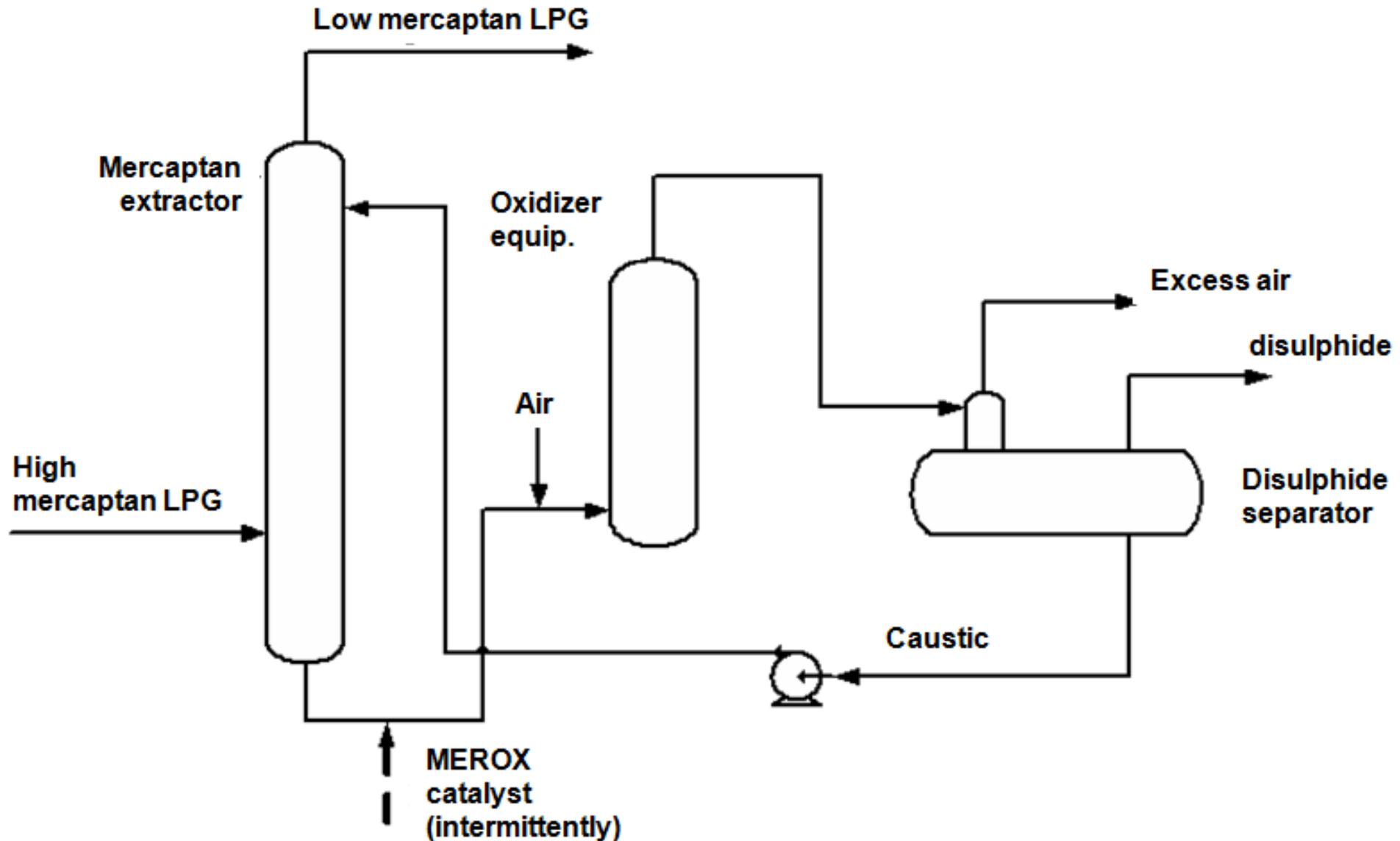


# LPG desulphurisation with **caustic**

- Two step, homogeneous catalytic process, conventionally called „**MEROX process**”
- **Advantage:** good for olefinic fractions (LPG from FCC, DCU)
- **Disadvantage:** caustic, catalyst containing waste water is produced
- 1. step: **desulphurisation**
  - **Theory:** absorption (liquid/liquid extraction)
  - Acidic mercapthanes are captured with caustic solution:
    - $(H_2S + 2NaOH \rightarrow Na_2S + 2H_2O)$
    - $RSH + NaOH \rightarrow RNa + H_2O$
- 2. step: **caustic regeneration**
  - **theory:** homogeneous catalytic oxidation
  - **Cobalt-ftalocianin** catalyst complex used to oxidise the mecapthanes into disulphides and regeneration of caustic
    - $(2Na_2S + 4H_2O + 2O_2 \rightarrow Na_2S_2O_3 + 2NaOH + 3H_2O)$
    - $2RNa + \frac{1}{2}O_2 + 2H_2O \rightarrow RSSR + 2NaOH + H_2O$



# Flowscheme of the **MEROX** process



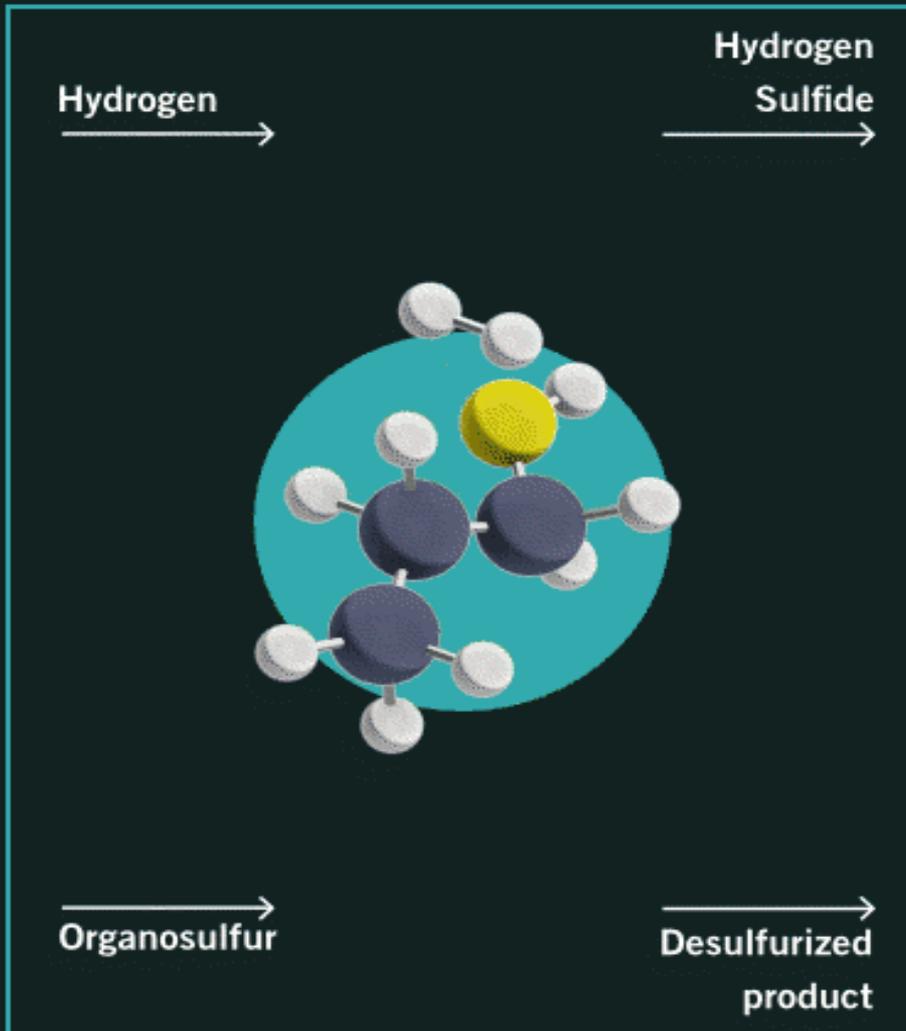
# Hydrotreatment of straight-run liquid fractions



# Hydrotreatment of straight-run liquid fractions

- **Theory:** heterogeneous catalytic desulphurisation
- **Similar** technology is used to desulphurised gasoline, petroleum, gasoil and vacuum distillate
- Good for straight-run **and** cracked streams
- Difference is in the **process parameters**
- Process needs **huge amount hydrogen** (in pure form)
  - Hydrogen plant (SMR-PSA)
  - Catalytic reformer (hydrogen is a byproduct here)

# HYDROTREATING

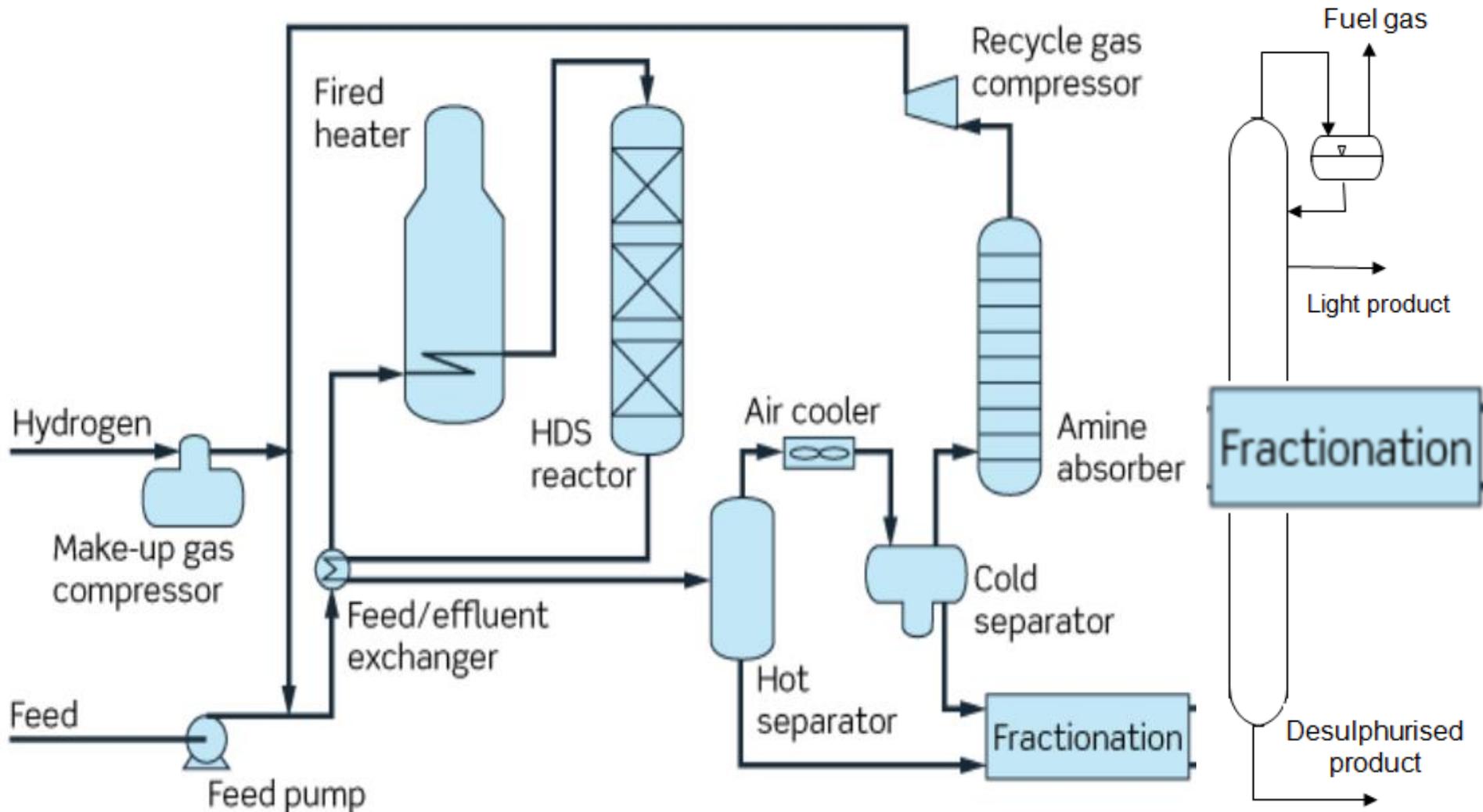


The distilled product may still contain undesirable elements, the most important of which is **sulfur**. Fuels containing sulfur, when burned, produce pungent sulfur dioxide.

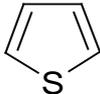
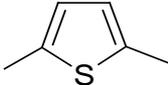
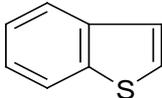
**Hydrotreating** removes sulfur by exposing the product to hydrogen gas as well as extreme heat and a catalyst. The hydrogen atoms bond with the sulfur, converting it into **hydrogen sulfide**. This hydrogen sulphide gas can then be removed via re-distillation.

In this example, the organosulfur compound **propanethiol** (C<sub>3</sub>H<sub>8</sub>S) is being converted into cleaner-burning **propane** (C<sub>3</sub>H<sub>8</sub>).

# Flowscheme of the **hydrotreaters**

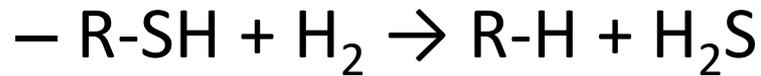


# Sulphuric species of **gasolines**

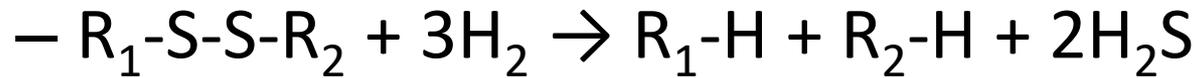
Compound	Formula	Boiling Point, °C
<b>Mercaptans</b>		
ethyl-mercaptan	$C_2H_5SH$	35,0
n-nonyl-mercaptan	$C_9H_{19}SH$	220
<b>Sulphides</b>		
dimethyl-sulphide	$CH_3-S-CH_3$	38
n-butyl-sulphide	$C_4H_9-S-C_4H_9$	188
<b>Disulphides</b>		
dimethyl-disulphide	$CH_3-S-S-CH_3$	109
ethyl-disulphide	$C_2H_5-S-S-C_2H_5$	153
<b>Thiophenes</b>		
thiophene		80
dimethyl-thiophene		135
benzothiophene		221

# Example reactions of gasoline desulphurisation

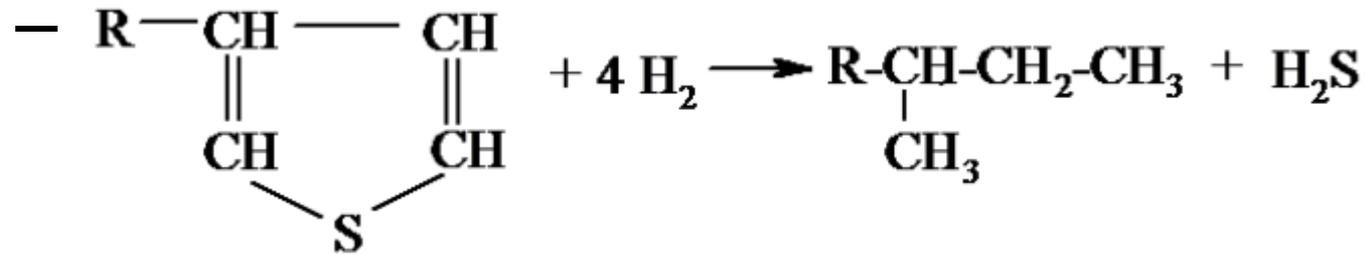
- **Mercaphanes:**



- **Disulphides:**



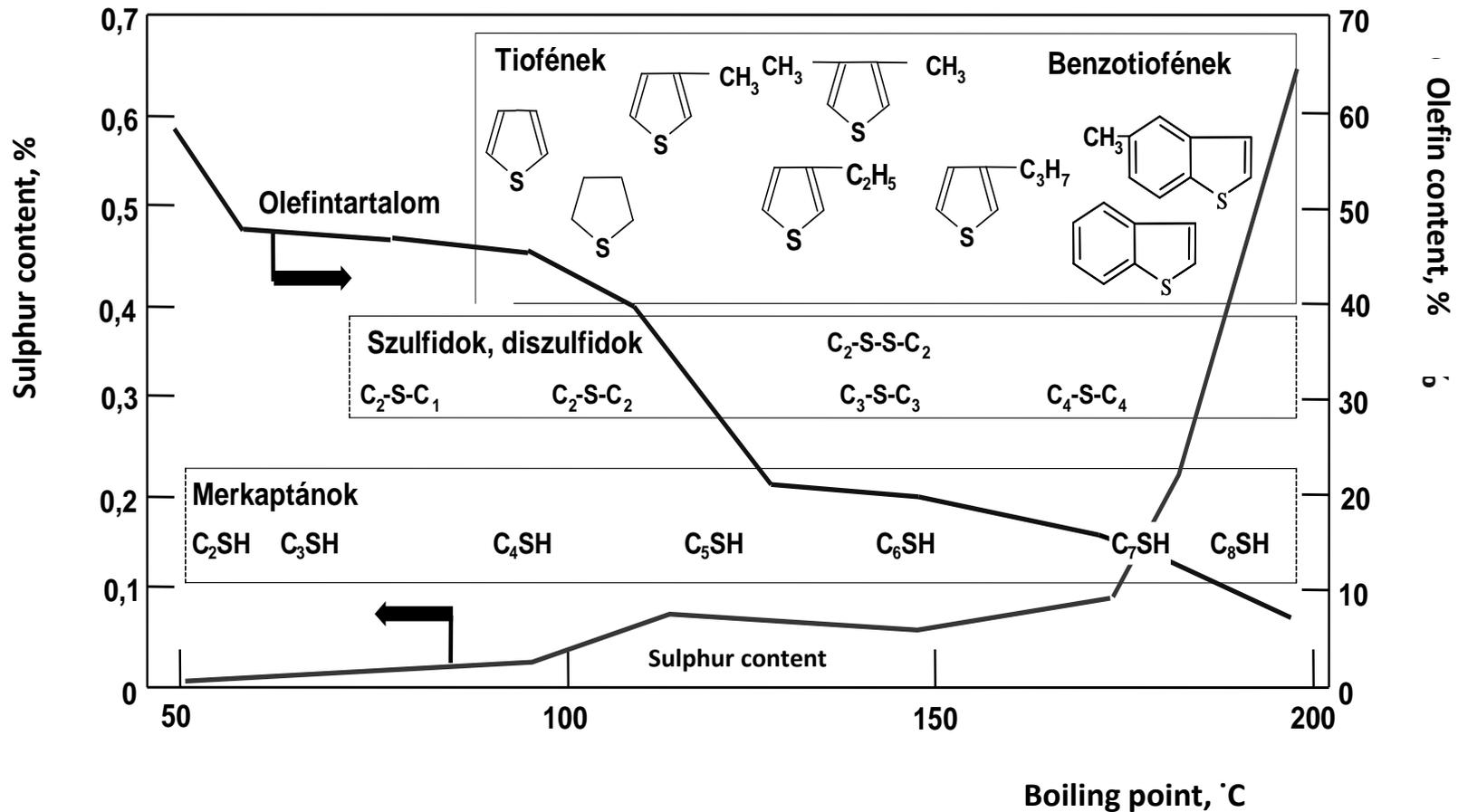
- **Thiophenes:**



# Challenges of cracked feed streams

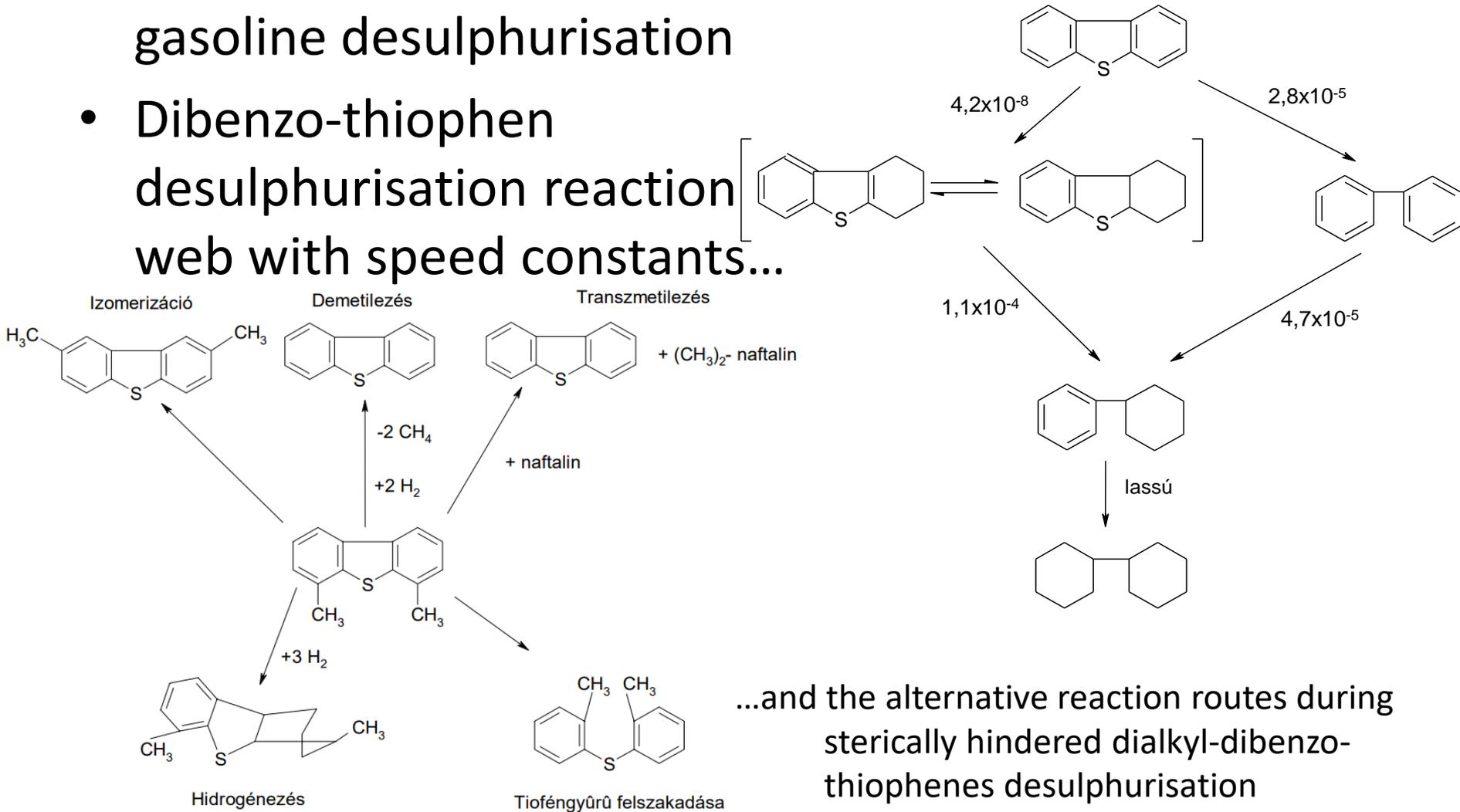
- **Potential feed stream**
  - Cracked (FCC) gasoline (appropriate RON – big quantity)
  - Coker (DCU) gasoline (not appropriate RON – medium quantity)
  - Pyrolysis gasoline (acetylenes present – small quantity)
- **Main challenge:** minimalization of olefine saturation
  - Olefines are high RON components
  - RON loss minimalization
  - Polymerization behavior of acetylenes are outstanding, during storage, they cause gum deposition problems (antioxidation additives are helpful)
- **Solutions**
  - Acetylene-selective hydrogenation
  - Fractionation and hydrogenation of heavier fraction only
  - Mild reaction conditions

# Typical composition of FCC gasoline

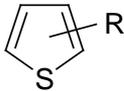
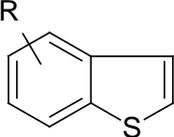
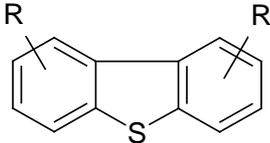
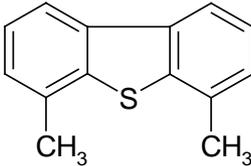


# Hydrotreatment of **petroleum and gasoil** fractions

- For desulphurization of simple sulphur compounds see gasoline desulphurisation
- Dibenzo-thiophen desulphurisation reaction web with speed constants...

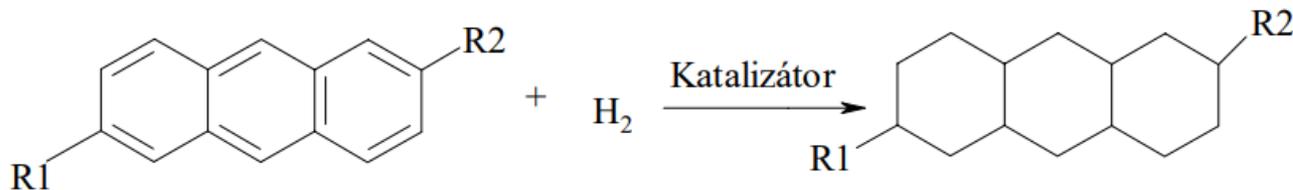


# Relative reactivity of thiophene derivatives

Sulphur compound	Formula	Relative reactivity
Thiophenes		1
Benzothiophenes		0,6
Dibenzothiophenes		0,04
4- and/or 6-methyl-dibenzothiophene		0,004

# Heteroatom removal of petroleum and gasoil fractions

- **Nitrogen** removal reactions:
  - Amines, nitriles, pirrol-derivatives, pyridine-derivatives:
    - pl.  $C_{18}H_{37}NH_2 + H_2 \rightarrow C_{18}H_{38} + NH_3$
    - In general: ammonia and saturated hydrocarbons are formed
- **Oxygen** removal reaction:
  - Phenol-derivatives, ketones, furane-derivatives, carboxyl-acids:
    - In general: water and saturated hydrocarbons are formed
- **Additional reactions:**
  - Aromatic ring saturation (mainly multiple-ring aromatics)

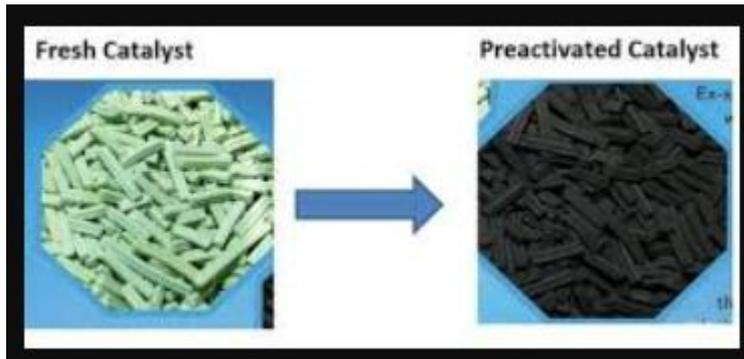


# Typical data of straight-run liquid fractions hydrotreatment

Feed	Gasoline	Petroleum	LAGO	HAGO	LVGO
<b>Parameters:</b>					
TBP cut points, °C	70-200	160-240	240-350	300-380	350-550
Sulphur, % (mg/kg)	(100-1000)	0,1-0,4	0,2-2	0,5-3	1-4
<b>Process parameters:</b>					
Temperature, °C	310-330	330-350	340-360	350-380	360-380
Pressure, bar	20-30	20-35	35-60	70-80	70-90
LHSV, h <sup>-1</sup>	4,0-6,0	2,0-4,0	1,0-3,0	0,8-2,0	0,5-2
H <sub>2</sub> /feed ratio, vol/vol	100-150	150-200	200-250	250-300	300-400
Product sulphur, mg/kg	<1	<1-50	≤10-50	≤10-500	≤50-500
Catalyst cycle life, month	48	→			24
Relative catalyst cost, 1/t	1	1,2	1,2	2	3,6

# Hydrotreating catalysts

- Catalyst consists typically
  - Transition metals: Ni, Co, Mo
  - On metal-oxide support: aluminium-oxide
  - Active in sulphide form
  - eg. **CoMo/Al<sub>2</sub>O<sub>3</sub>**, **NiMo/Al<sub>2</sub>O<sub>3</sub>**

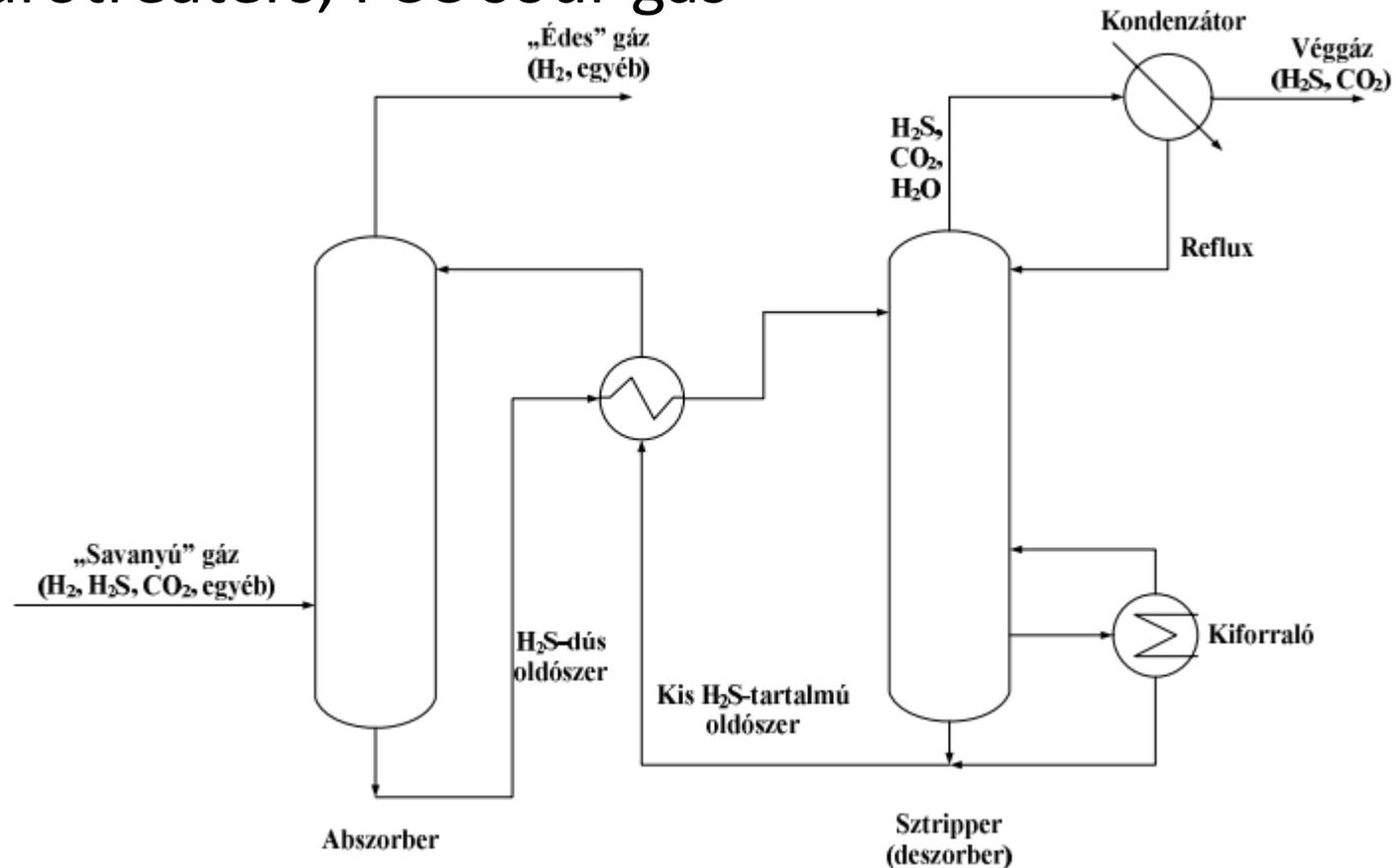


## 2. Sulphur removal and production from hydrogen-sulphide containing gases



# Hydrogene-sulphide removal from gas mixtures

- **Theory:** gas/liquid extraction
- **Feedstock:** fuel gas,  $H_2S$  rich gases from hydrotreaters, FCC sour gas



# Used absorbents

- Chemisorption reaction on MDEA:



Oldószer	MEA	DEA	MDEA
<u>Molekulatömeg</u>	61	105	119
Koncentráció (tf%)	15	30	50
Minimális H <sub>2</sub> S terhelés (n <sub>H2S</sub> /n <sub>amin</sub> )	0,05	0,02	0,01
Maximális H <sub>2</sub> S terhelés (n <sub>H2S</sub> /n <sub>amin</sub> )	0,6	0,6	0,5
Kapacitás (H <sub>2</sub> S/dm <sup>3</sup> )	1,77	2,18	2,77

MEA: mono-etanol-amin

DEA: di-etanol-amin

MDEA: metil-di-etanol-amin

# Sulphur production from hydrogen-sulphide – the **Claus process**

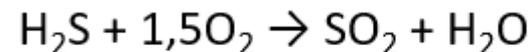
- **Theory:**

- 1. step: **partial oxidation** (stoichiometric 1/3)
- 2. step: **catalytic conversion**
- Conversion **efficiency**: 99,5% <

- **Reactions:**

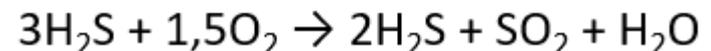
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(1) Részleges égés az égetőkamrában



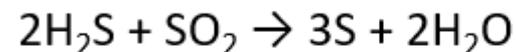
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vagy (az elégetlen H<sub>2</sub>S-t is figyelembe véve)



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(2) Claus reakció az égetőkamrában és a katalitikus konverterben

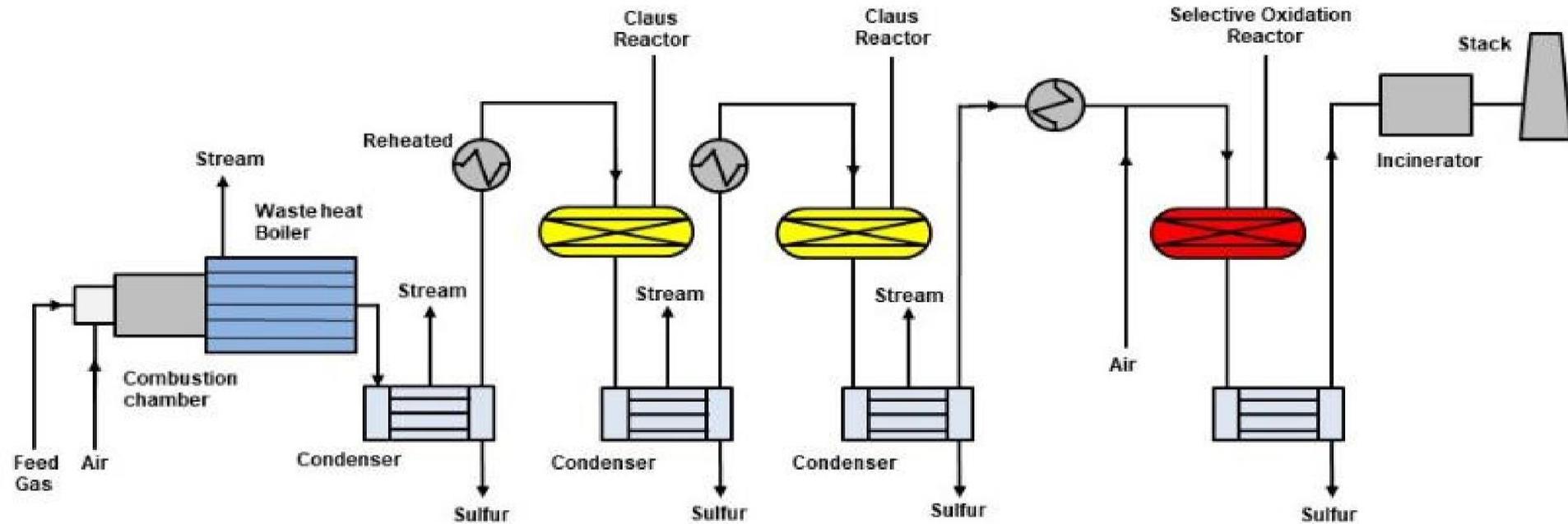


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**(1+2) Bruttó reakció**



# Flowscheme of the Claus process

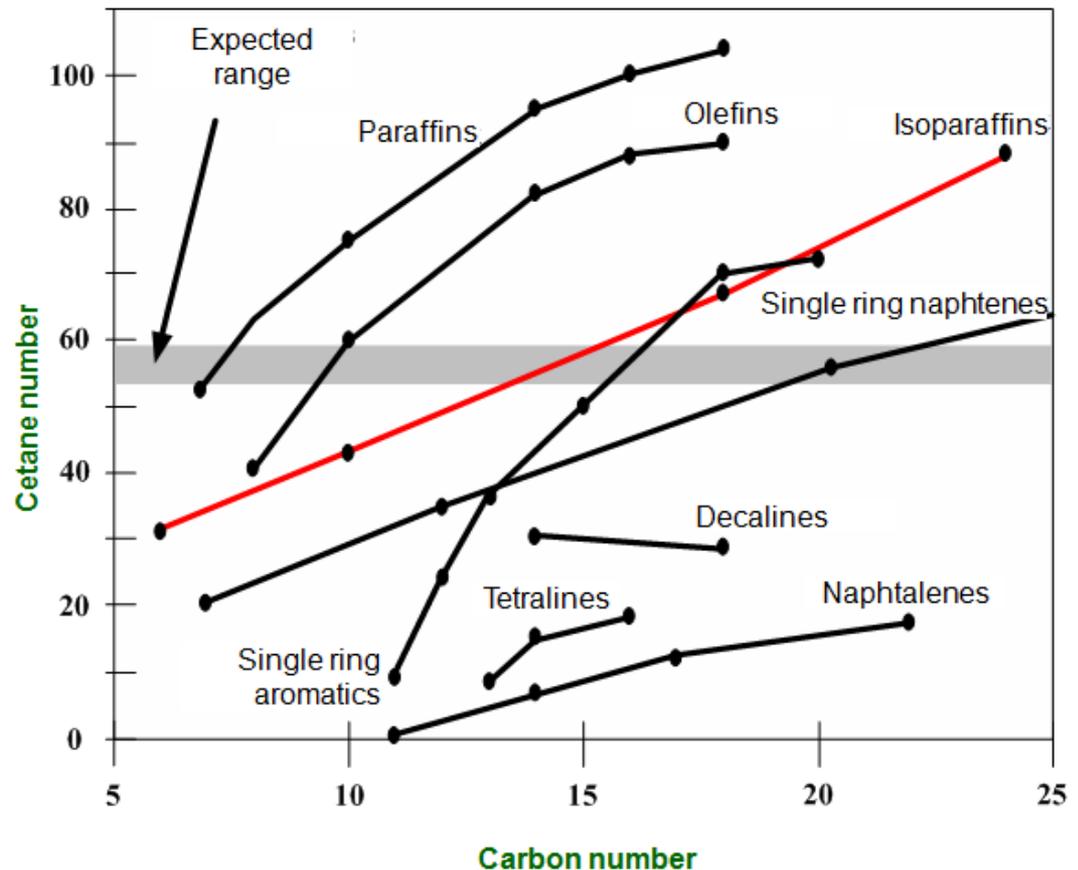


# 3. Quality improvement of gasoil fractions



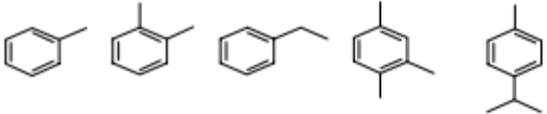
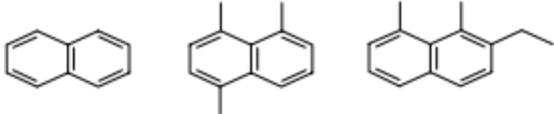
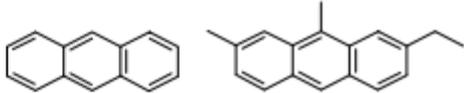
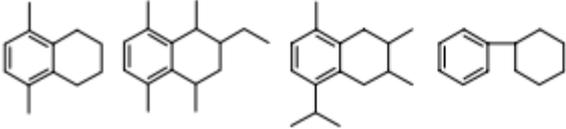
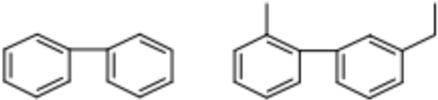
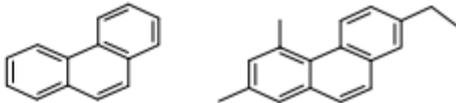
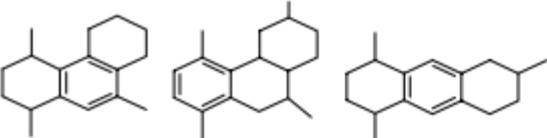
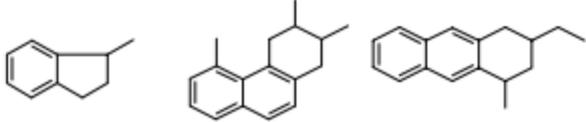
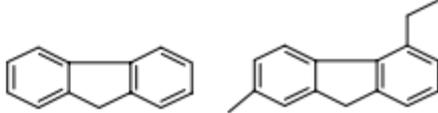
# A. Aromatic saturation of gasoils

- Goal of aromatic saturation
  - **Cetane number** of the polyaromatic molecules are low:
    - cetane number of gasoil increases with saturation
  - Burning of polyaromatic molecules are **not complete**
    - with saturation the particulate emission may be decreased (older diesel cars exhaust gas)





# Some examples of polyaromatic molecules

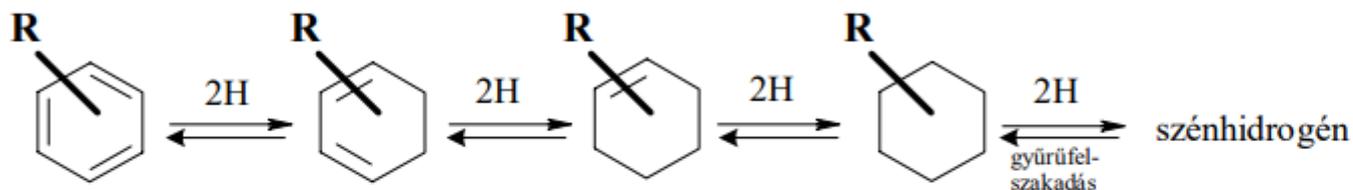
Egy-gyűrűs aromások	Kétgyűrűs aromások	Háromgyűrűs aromások
<p data-bbox="54 475 382 518"><b>- alkil-benzolok</b></p> 	<p data-bbox="666 475 1300 518"><b>- naftalinok és alkil-naftalinok</b></p> 	<p data-bbox="1342 475 1609 518"><b>- antracének</b></p> 
<p data-bbox="54 761 542 803"><b>- benzo-cikloparaffinok</b></p> 	<p data-bbox="666 761 884 803"><b>- bifenilek</b></p> 	<p data-bbox="1342 761 1628 803"><b>- fenantrének</b></p> 
<p data-bbox="54 1046 575 1089"><b>-benzo-dicikloparaffinok</b></p> 	<p data-bbox="666 1046 1242 1089"><b>- nafténaromások (indének)</b></p> 	<p data-bbox="1342 1046 1580 1089"><b>- fluorének</b></p> 

# Saturation of aromatic hydrocarbons

## Erősen exoterm reakció

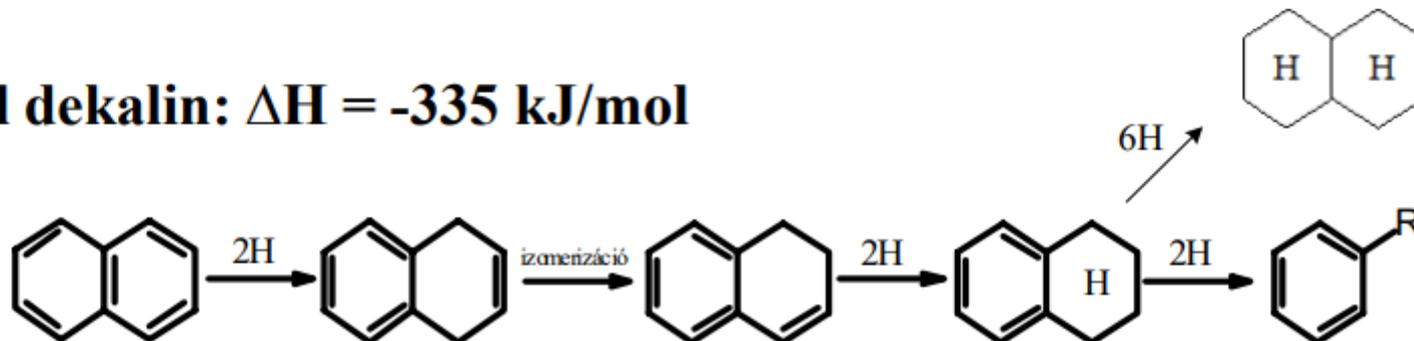
### □ alkil-benzolból alkil-ciklohexán:

toluol  $\rightarrow$  metil-ciklohexán:  $\Delta H = -205$  kJ/mol  
etil-benzol  $\rightarrow$  etil-ciklohexán :  $\Delta H = -202$  kJ/mol  
kumol  $\rightarrow$  2-ciklohexil-propán: :  $\Delta H = -184$  kJ/mol

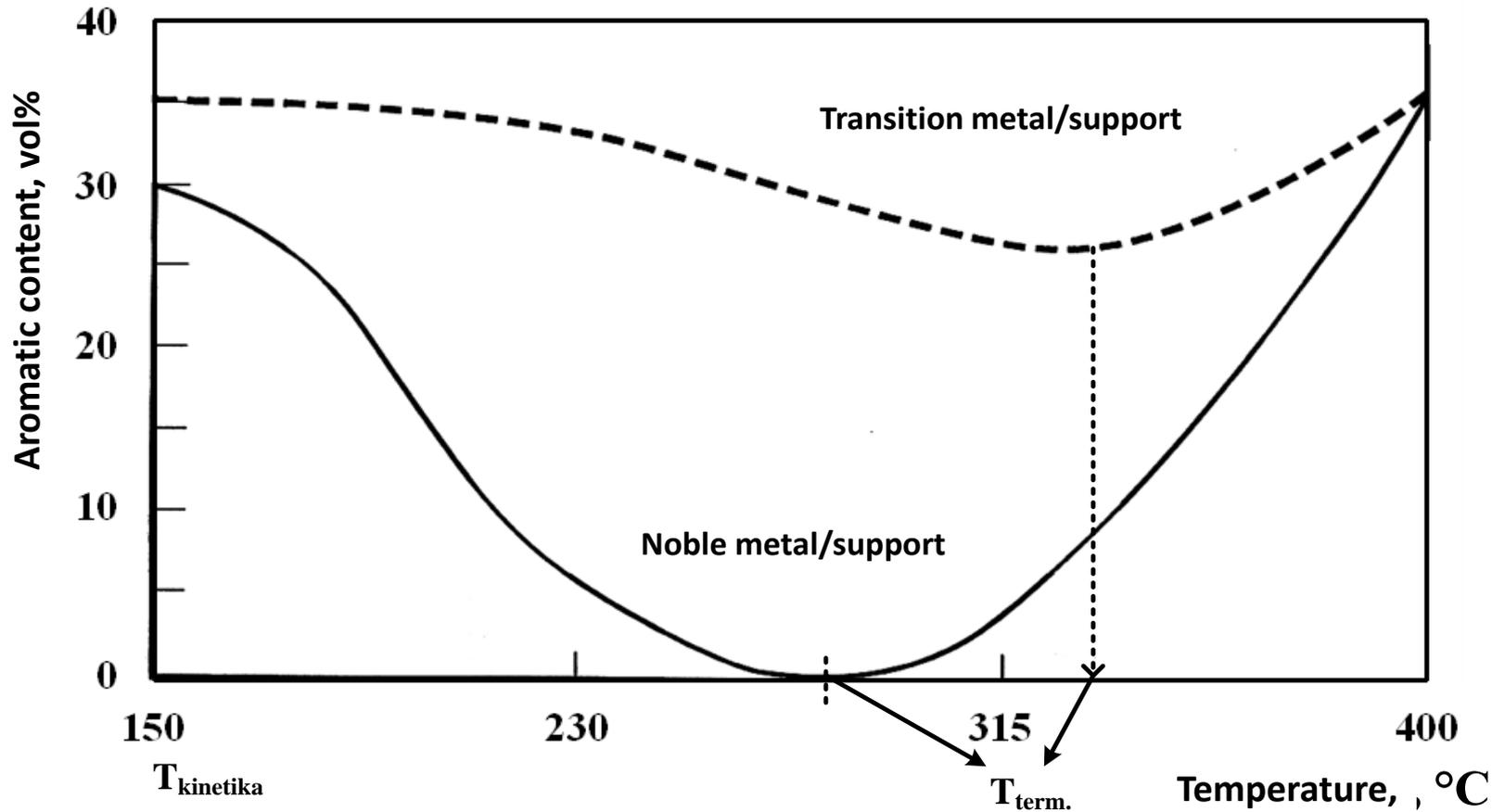


(a reakcióhő az alkilánc méretének növekedésével csökken; egyre kevésbé exoterm a reakció)

### □ naftalinból dekalin: $\Delta H = -335$ kJ/mol



# Effect of reaction temperature on aromatic saturation



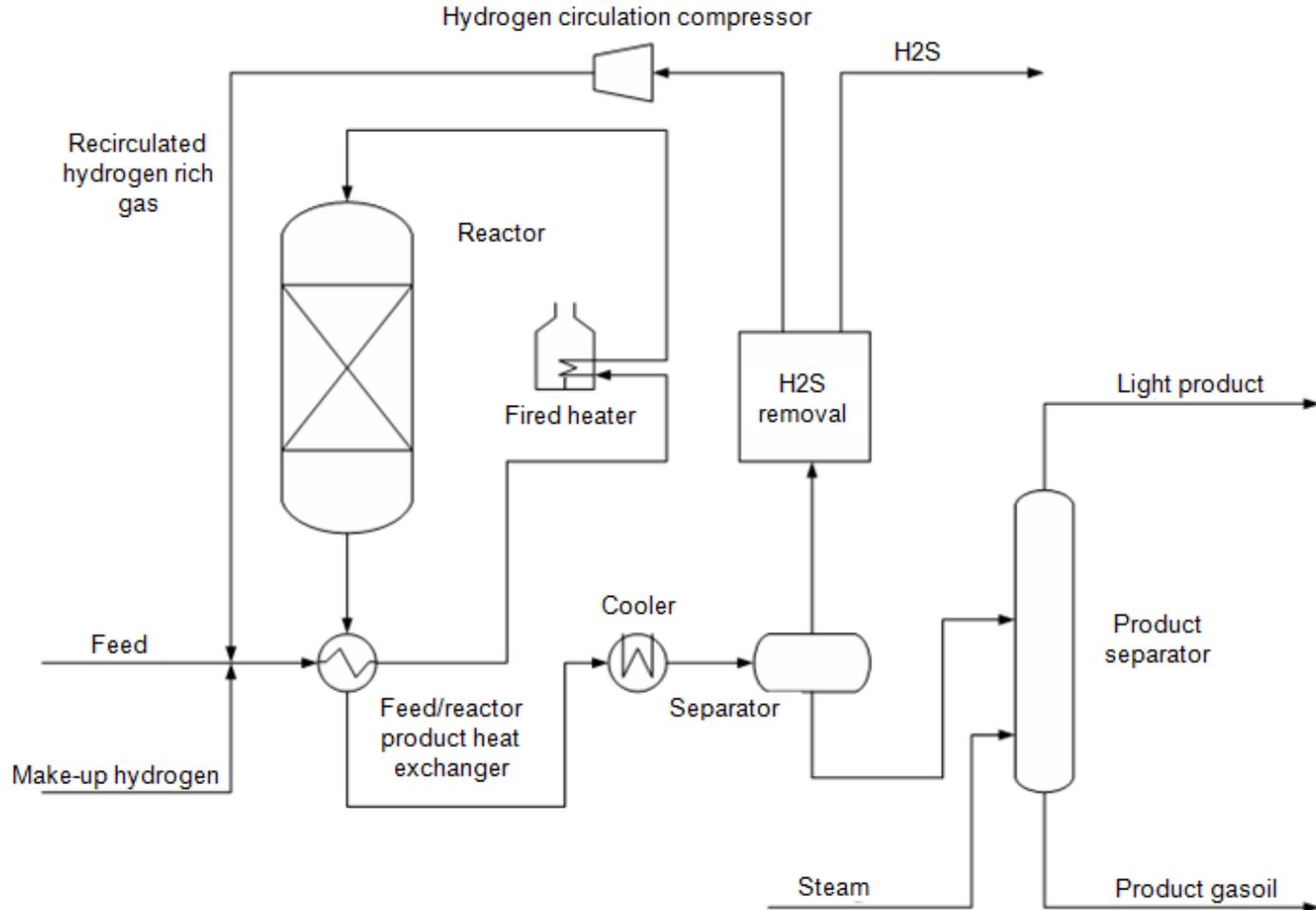
# Catalysts of aromatic hydrogenation

- **High sulphur tolerance** catalysts (feed sulphur content  $250 <$  mg/kg)
  - Mo, W (VI. group) és Co, Ni (VIII. group), in sulphide state, on  $\gamma$ - $\text{Al}_2\text{O}_3$  support
    - Activity order:  $\text{Mo} > \text{W} \gg \text{Ni} > \text{Co}$
  - $\text{NiMo}/\text{Al}_2\text{O}_3$ ,  $\text{CoMo}/\text{Al}_2\text{O}_3$ ,  $\text{NiW}/\text{Al}_2\text{O}_3$  in sulphide state
    - Activity order:  $\text{NiW} > \text{NiMo} > \text{CoMo} > \text{CoW}$
  - Only partial aromatic saturation (up to max. 50-80 %; min. 60 bar  $\text{H}_2$  partial pressure)
- **Low sulphur tolerance** catalysts (feed sulphur content  $< 250$  mg/kg, rather  $< 10$ - $20$  mg/kg)
  - Pt or Pd amorphous  $\text{Al}_2\text{O}_3$ - $\text{SiO}_2$ , or acidic (USY) support
  - High aromatic saturation (up to 95 %;  $T_{\text{max}}$ : 300-310 °C,  $p_{\text{H}_2}$ : 25-40 bar)

# Industrial solutions

- **Differences** between the different solutions
  - In the order of heteroatom removal and aromatic saturation (parallel or one after the other)
  - In the number of applied number of reactors
  - In the applied catalysts
  - In the position of the catalysts (eg. separated beds)
  - In the cooling mode
  - In the applied process parameters
- The main classification of the industrial processes
  - Single step
  - Two step processes

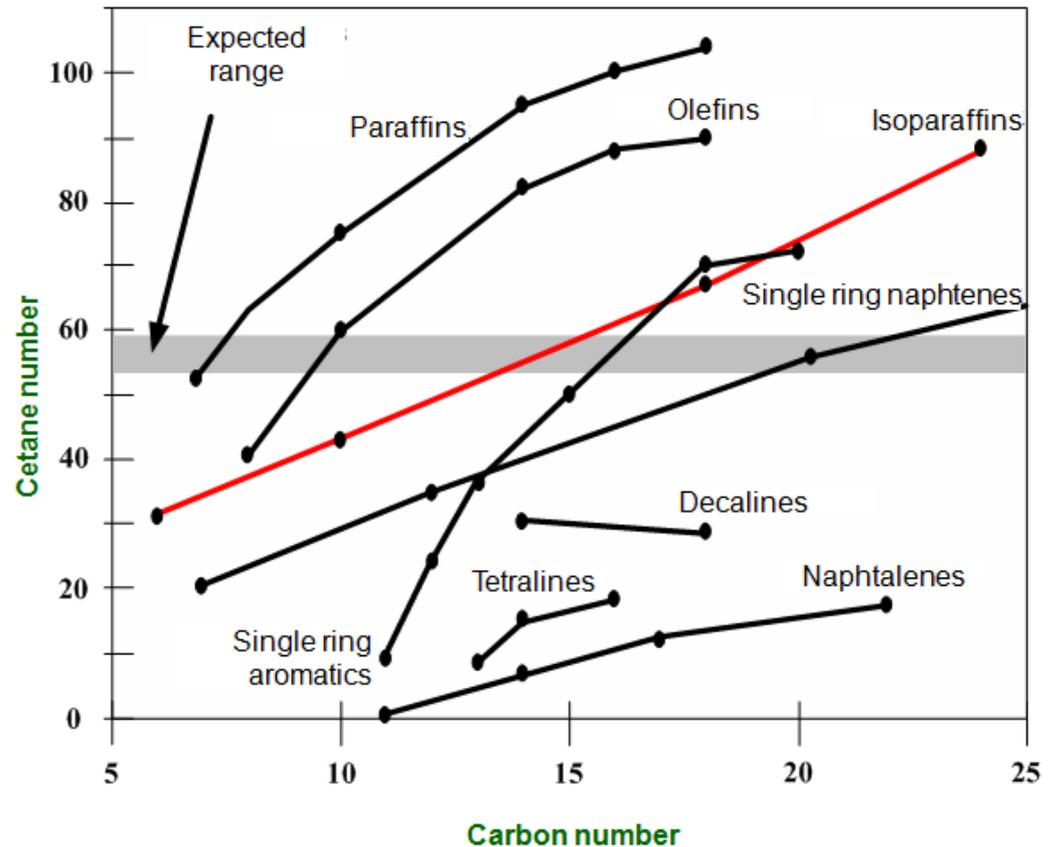
# Single step technology



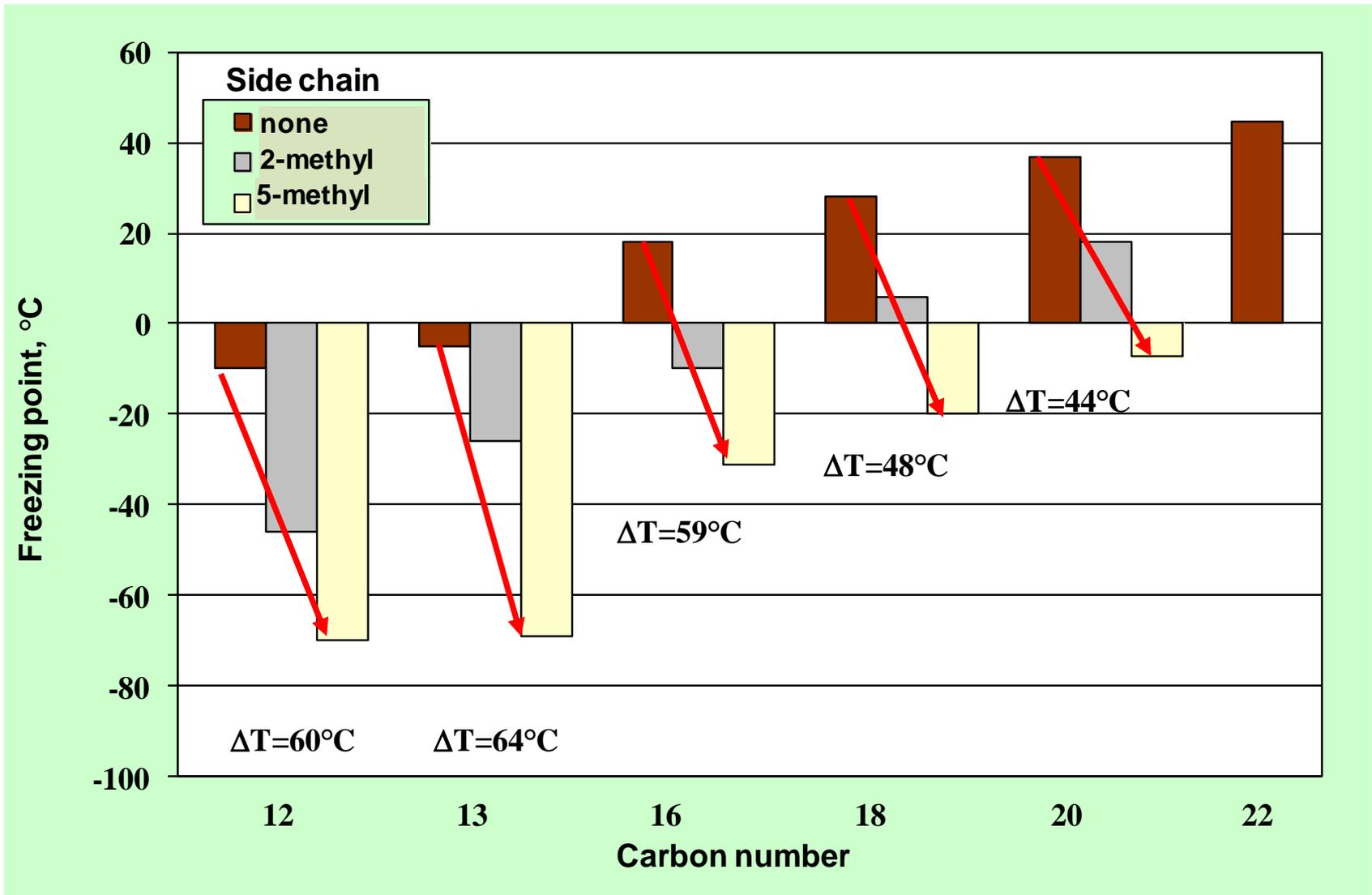


# B. Conversion of **paraffin content** of gasolines

- Goal of paraffin conversion
  - Freezing point of n-paraffins are high – at low temperature they crystallize and plug the fuel lines
- Freezing point decrease options:
  - Selective hydrocracking
  - Selective isomerisation
  - Combination of above
- Measurement:
  - Cold filter plugging point (CFPP)



# Effect of **izomerisation** on freezing point







# The End

